

Parabolic Cylinder Analysis

Dave McGinnis

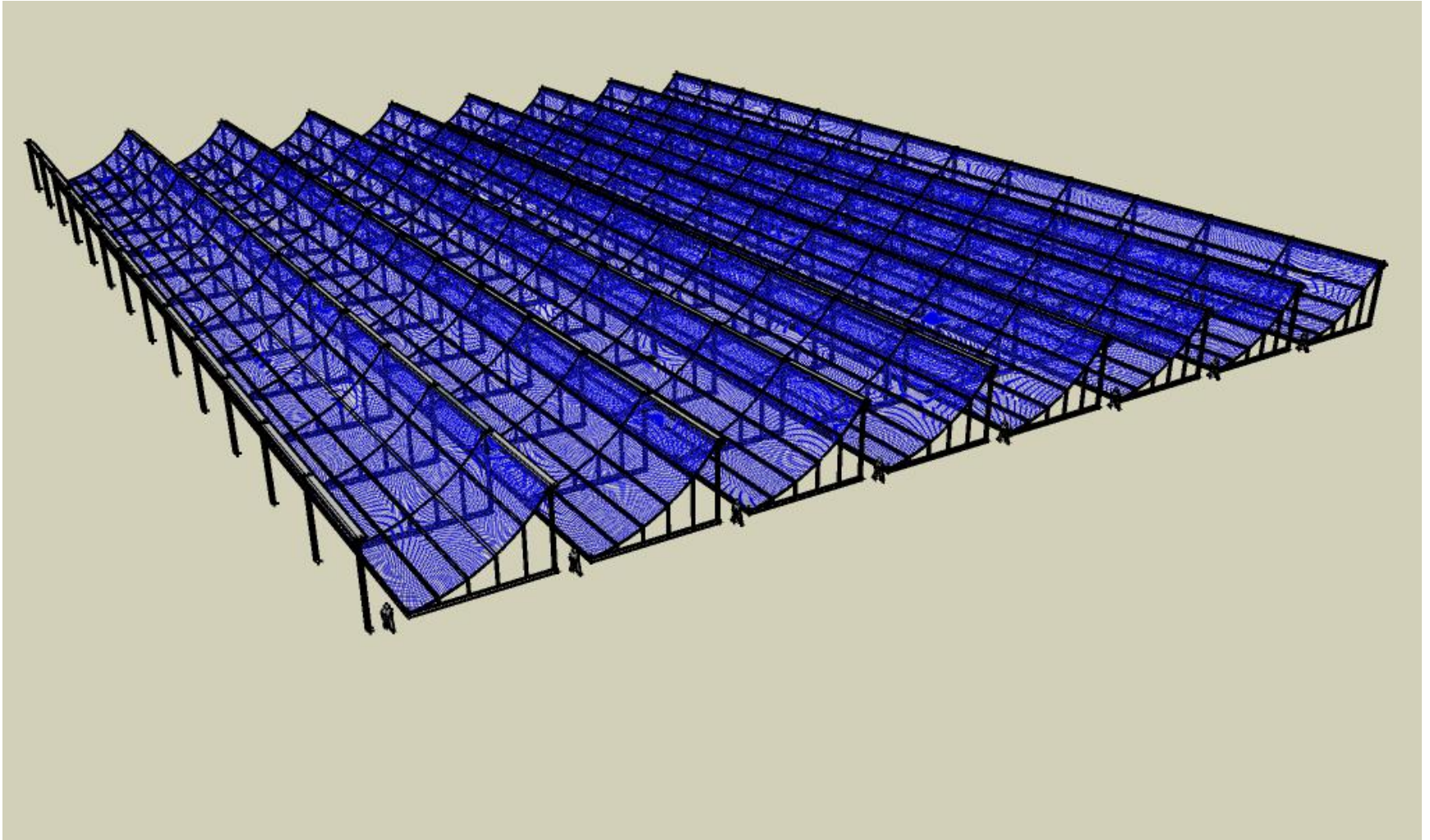
Fermilab

October 3, 2008

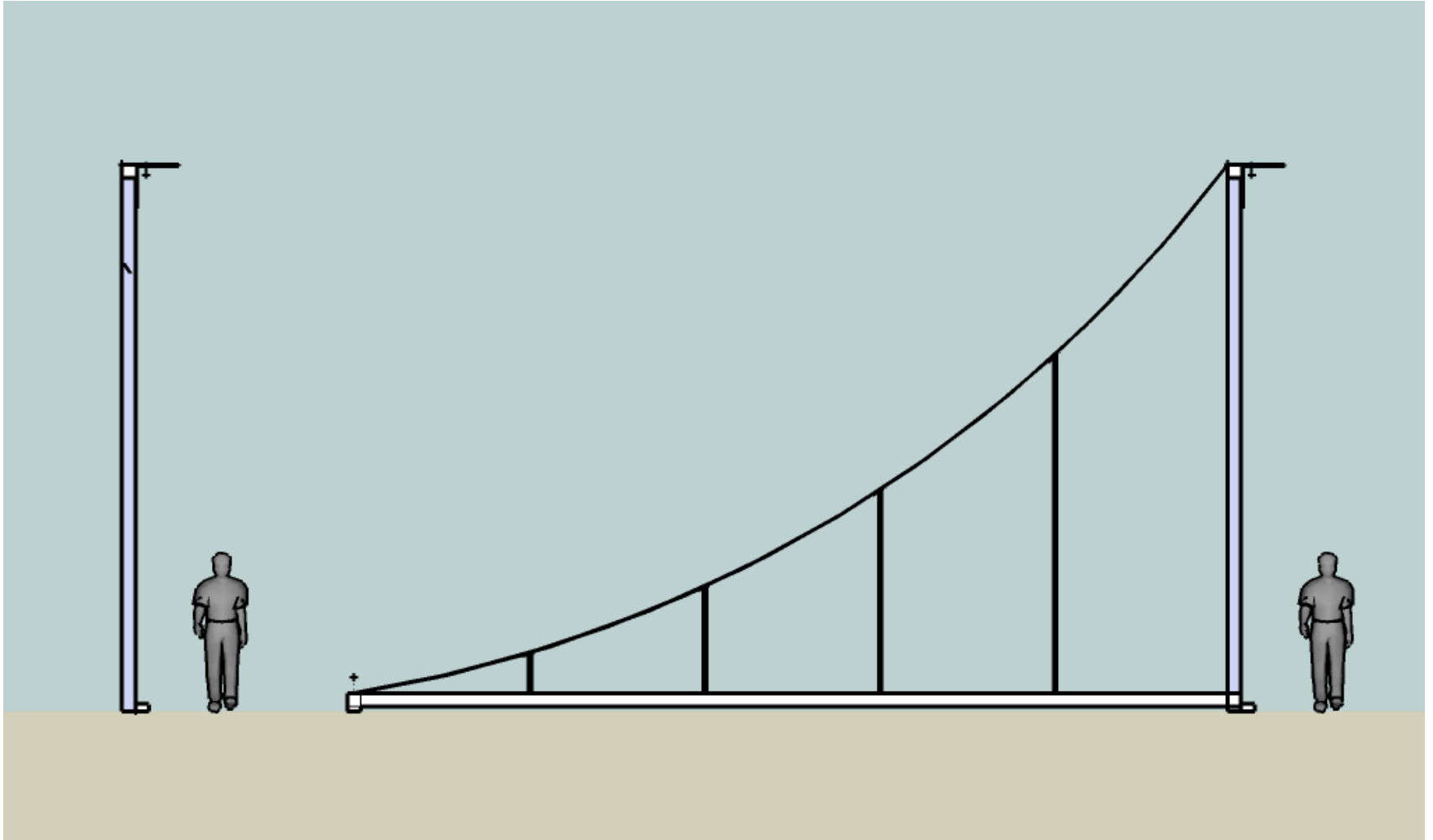
Design Parameters

- Number of cylinders = 8
- Cylinder length = 130 m
- Cylinder width = 12.5 m
- Cylinder Transverse beam width < 8 x 15 arc-min

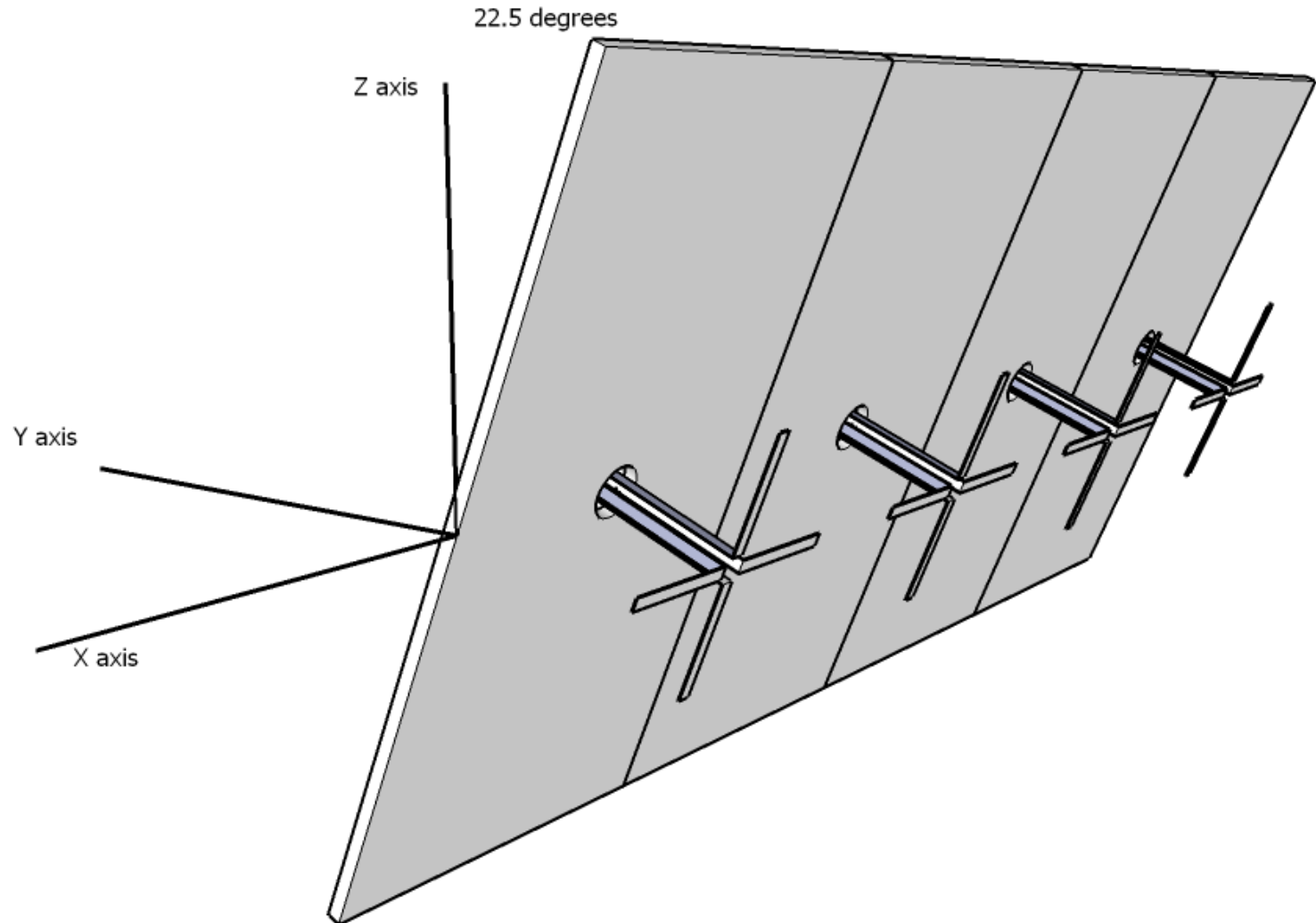
Telescope Layout



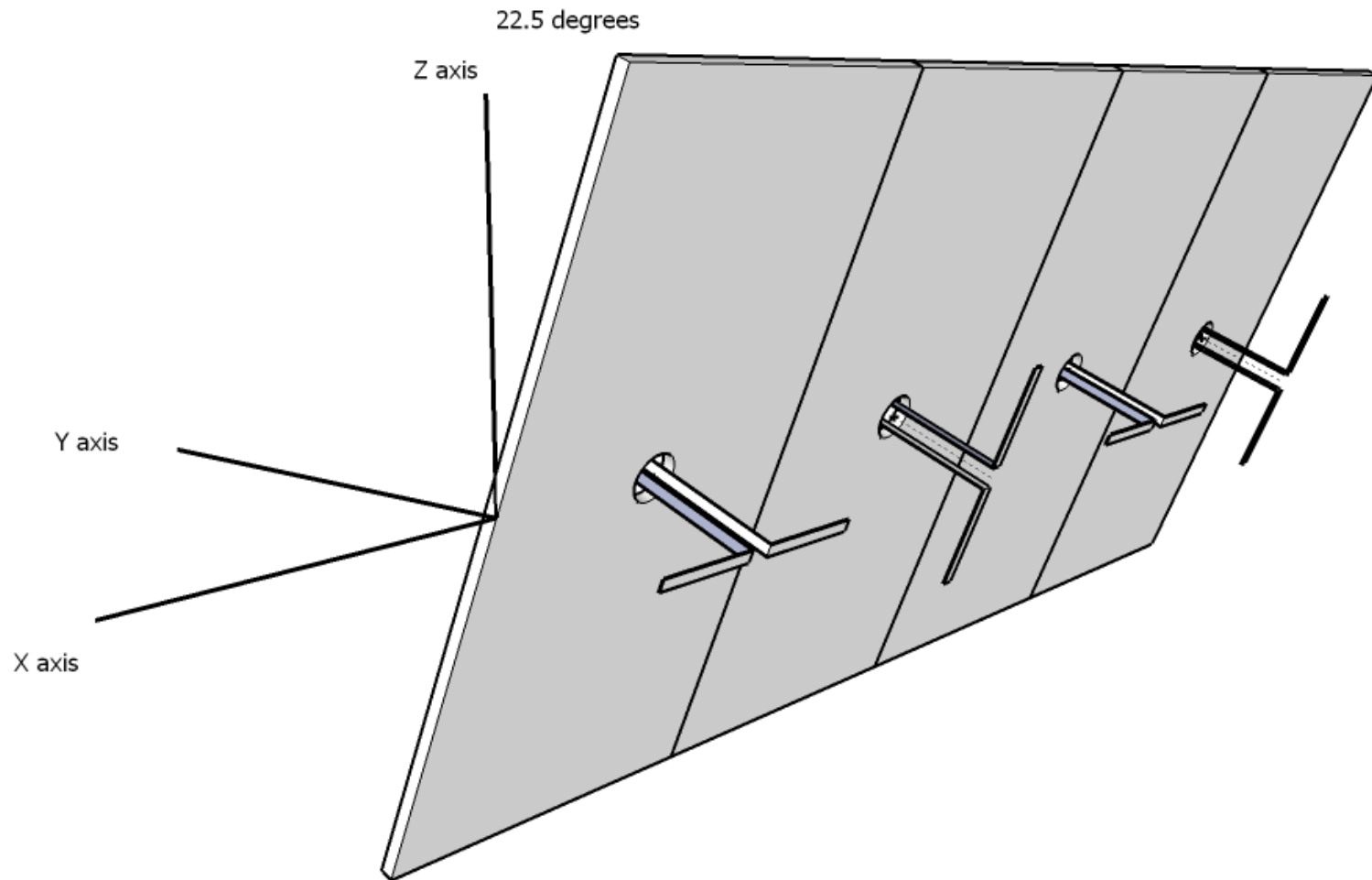
Cylinder Cross-Section



Simple Telescope Feed (first attempt)



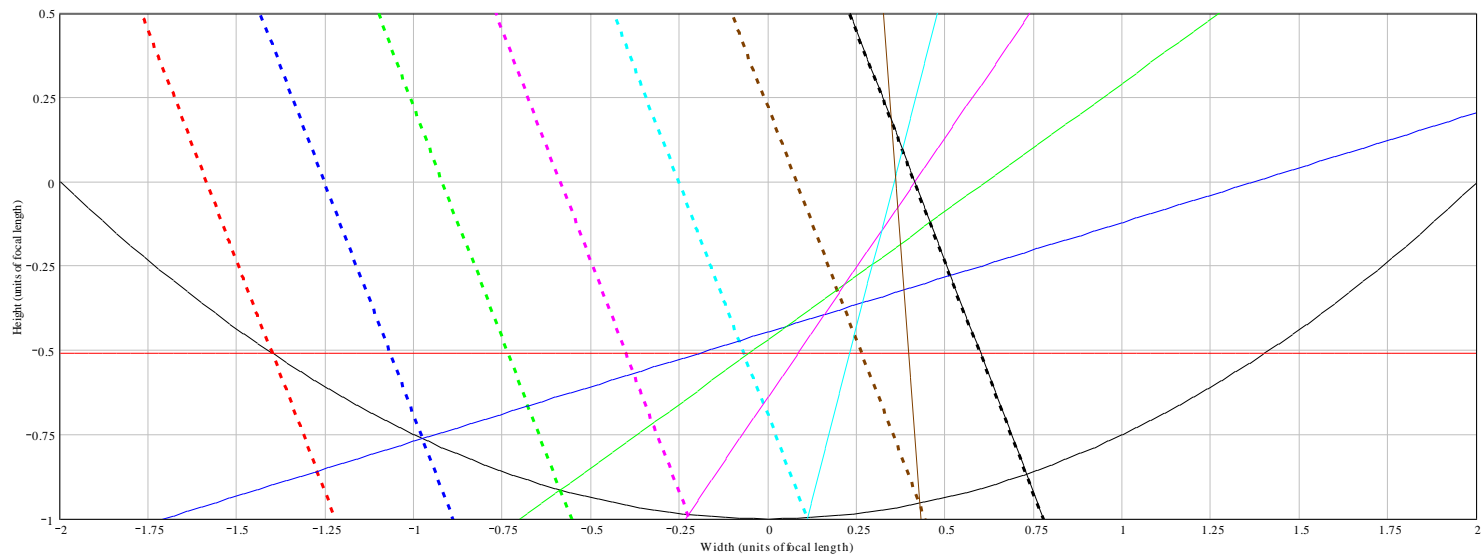
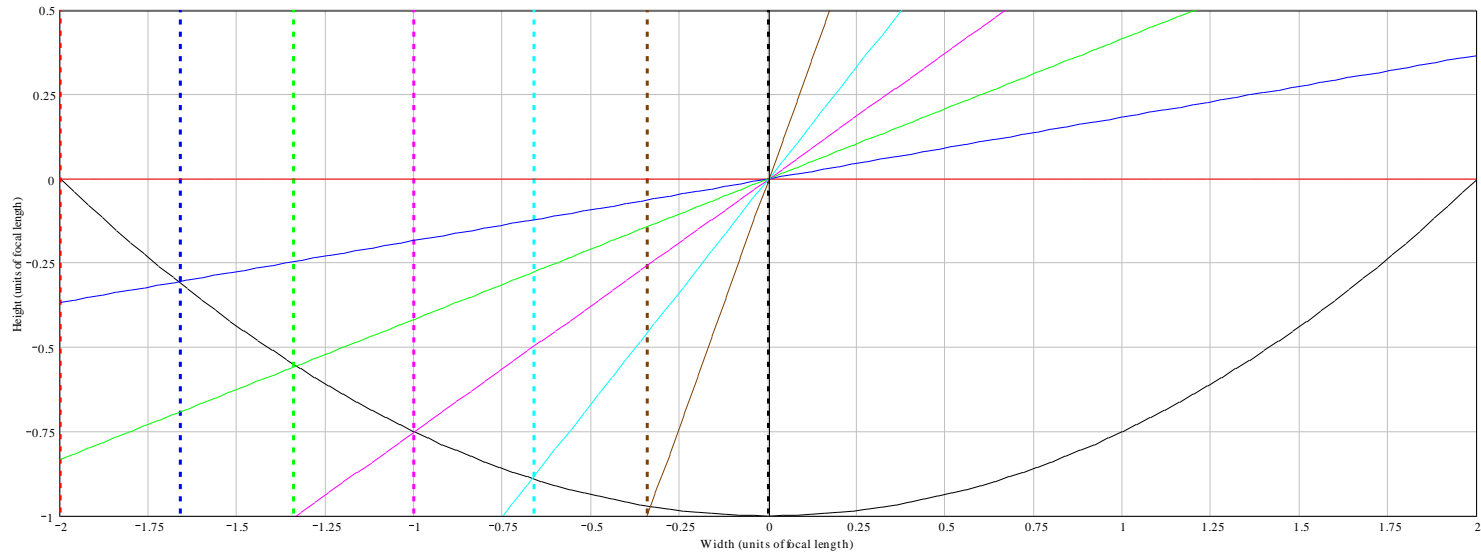
Alternating Telescope Feed



Offset-Fed Telescope

- Concern about double bounce modulation between dish and feed will cause significant ripple in the antenna pattern.
- Would like feed to be hidden by dish to shield from RFI sources.
- Small f-ratio exaggerates focus errors
 - Beam must be parallel to primary axis
 - Cut >50% of dish away

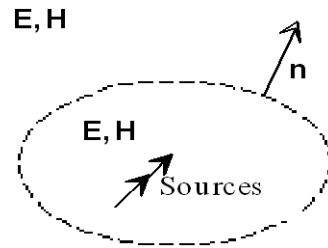
Offset-Fed Telescope



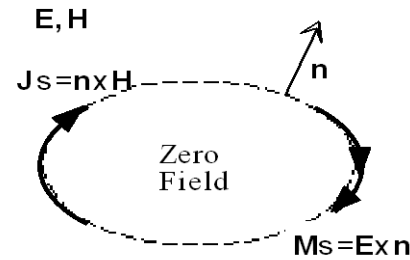
Cylinder Simulations

- Physical Optics Approximation
- The antenna dish reflects a scattered field so that the total tangential electric field on the dish is zero. $\vec{E}_{Total} = \vec{E}_{inc} + \vec{E}_{scat}$
- On the surface of the dish: $\hat{n} \times \vec{E}_{inc} = -\hat{n} \times \vec{E}_{scat}$
- If the incident field on the dish surface is known, then the scattered field on the dish surface is also known

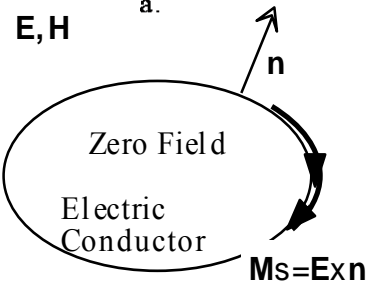
Physical Optics Approximation



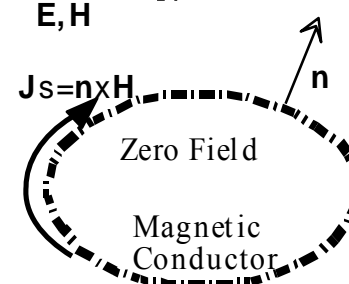
a.



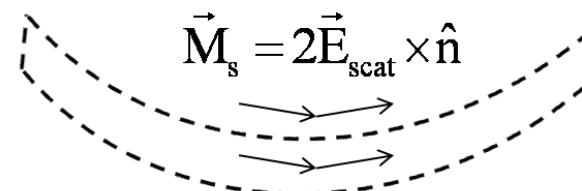
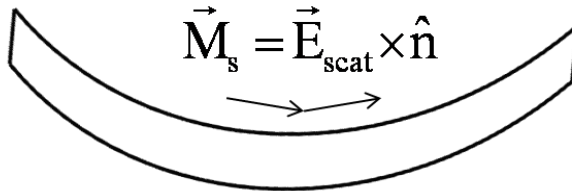
b.



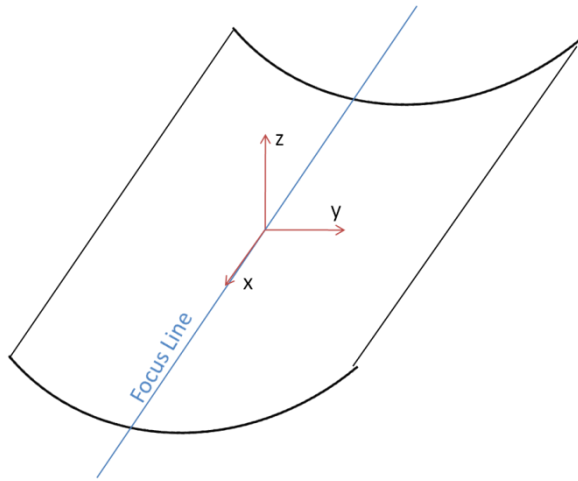
a.



b.

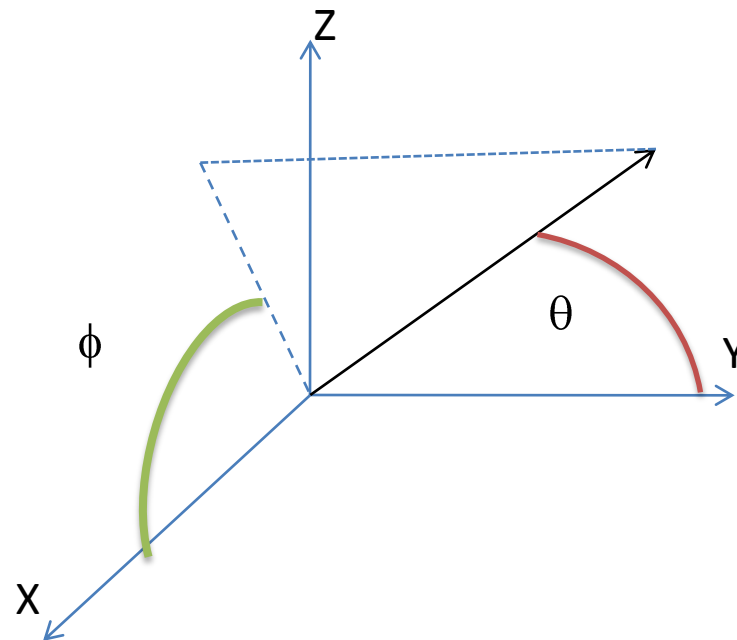


Telescope Coordinate System

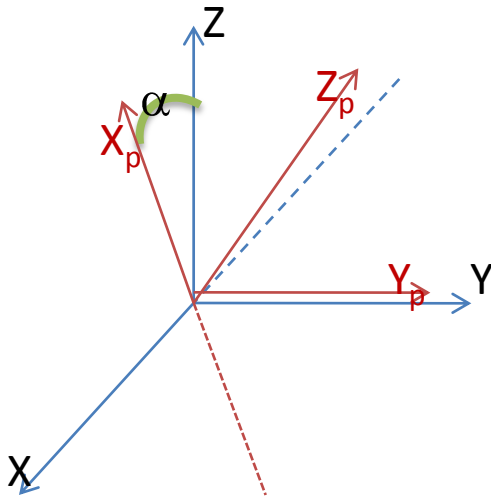


$$D(\phi, \theta) = \frac{U(\phi, \theta)}{\frac{1}{4\pi} \iint U(\phi, \theta) \sin(\theta) d\theta d\phi}$$

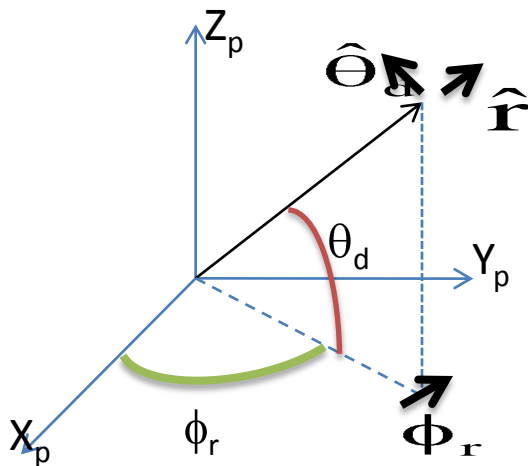
$$U(\phi, \theta) = \frac{1}{2} \text{Re}\{\vec{E} \times \vec{H}^*\} \cdot \hat{r} R^2$$



Polarization



Celestial coordinate system (in red) with respect to telescope coordinate system. The angle α equal to the latitude of the telescope location



Celestial Coordinate system defined by declination angle, θ_d , and right ascension angle, ϕ_r .

$$\begin{aligned} \hat{\theta}_d = & -(\sin(\alpha)\sin(\theta_d)\cos(\phi_r) + \cos(\alpha)\cos(\theta_d))\hat{x} \\ & +(\sin(\theta_d)\sin(\phi_r))\hat{y} \\ & +(-\cos(\alpha)\sin(\theta_d)\cos(\phi_r) + \sin(\alpha)\cos(\theta_d))\hat{z} \end{aligned}$$

$$\begin{aligned} \hat{\phi}_r = & -(\sin(\alpha)\sin(\phi_r))\hat{x} \\ & +(\cos(\phi_r))\hat{y} \\ & -(\cos(\alpha)\sin(\phi_r))\hat{z} \end{aligned}$$

Directivity

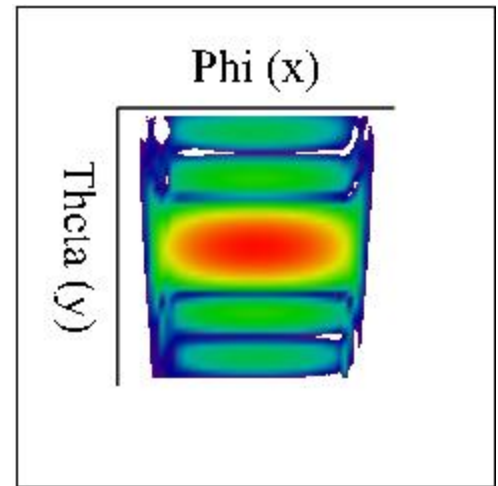
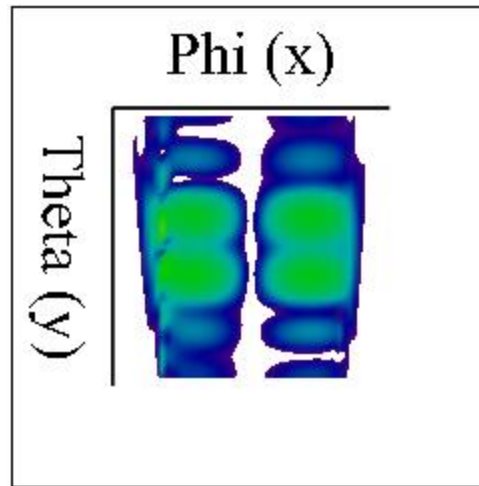
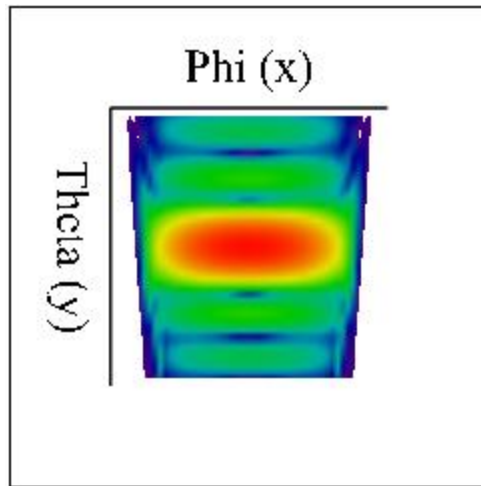
$$D(\phi, \theta) = \frac{U(\phi, \theta)}{\frac{1}{4\pi} \iint U(\phi, \theta) \sin(\theta) d\theta d\phi}$$

$$\Omega_A = \frac{4\pi}{D_{\max}}$$

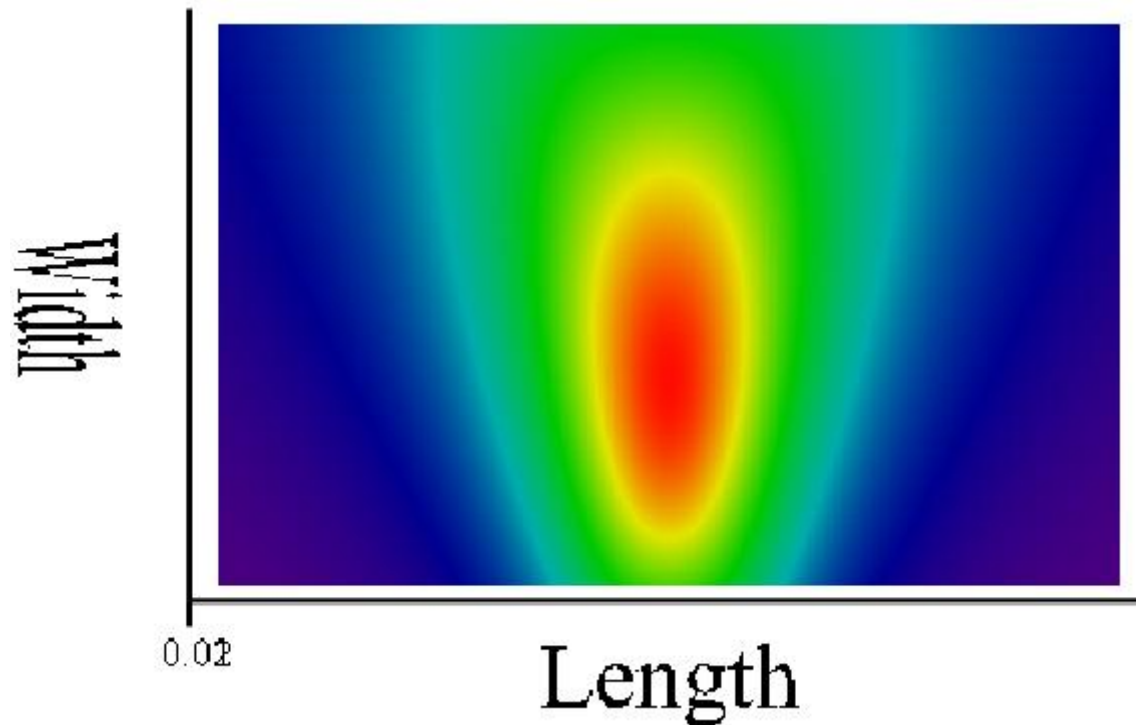
$$A_{em} = \frac{\lambda^2}{\Omega_A}$$

$$L_{em} = \frac{A_{em}}{W}$$

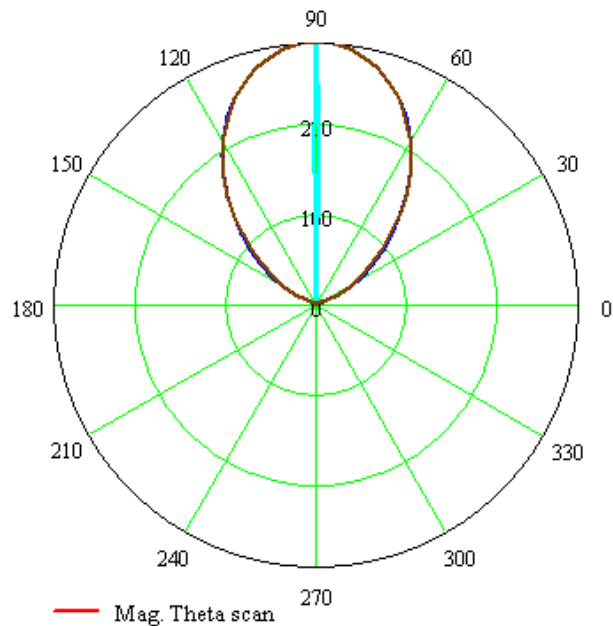
Y-Z Polarization Results



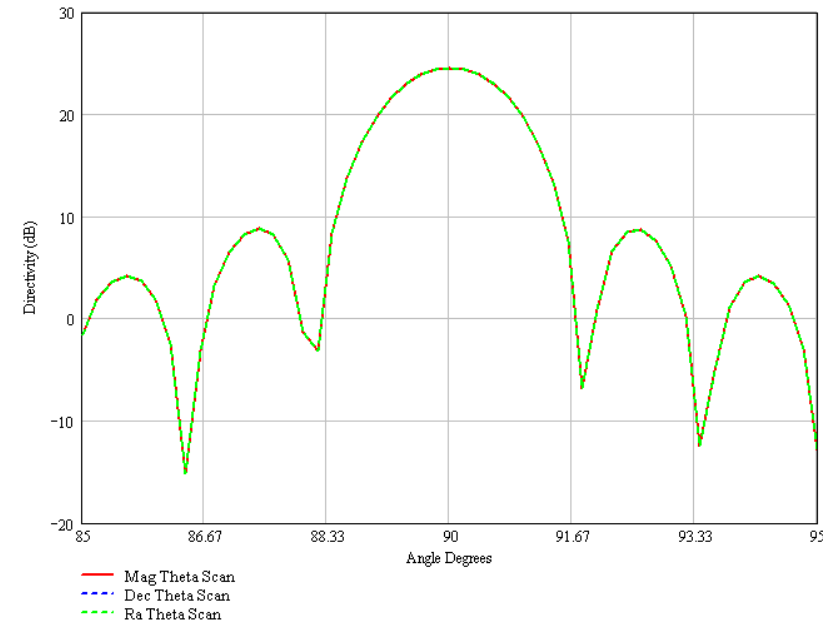
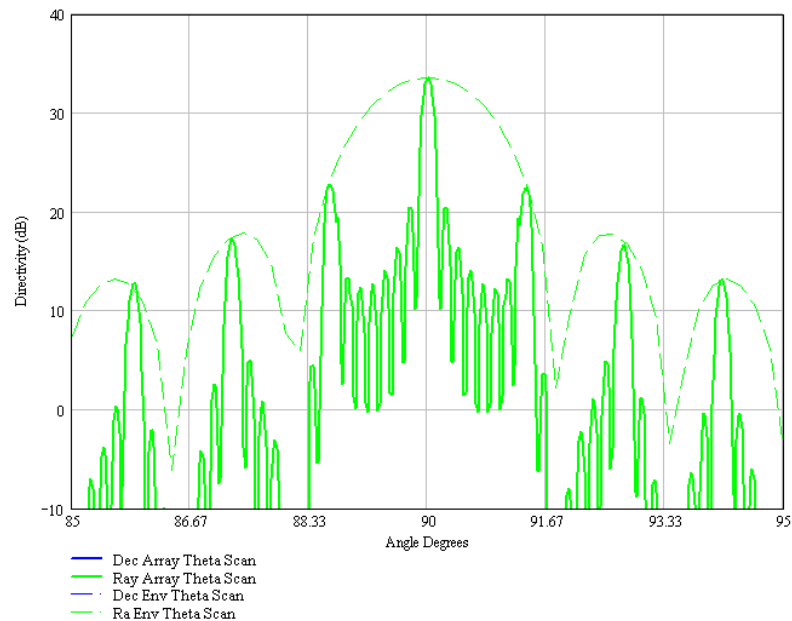
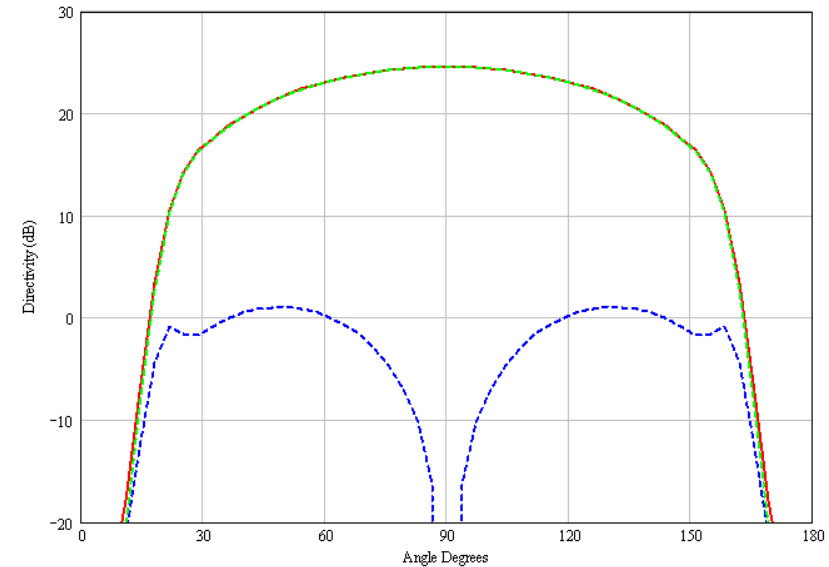
eMagLog



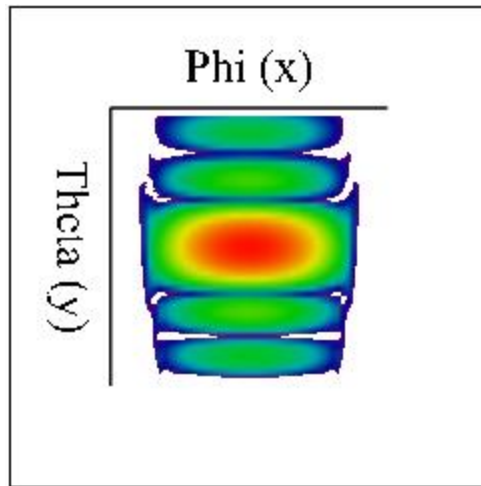
Y-Z Polarization Results



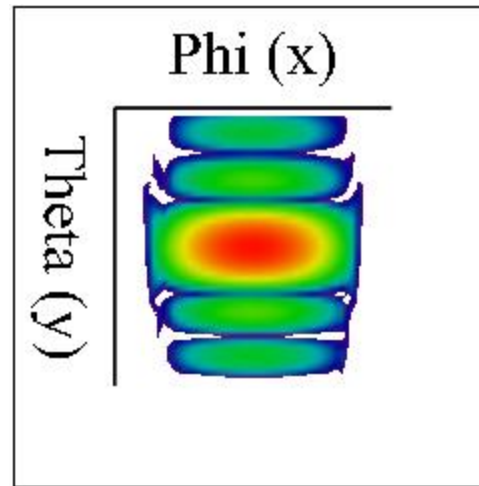
$$\frac{L_{em}}{\lambda} = 0.687$$



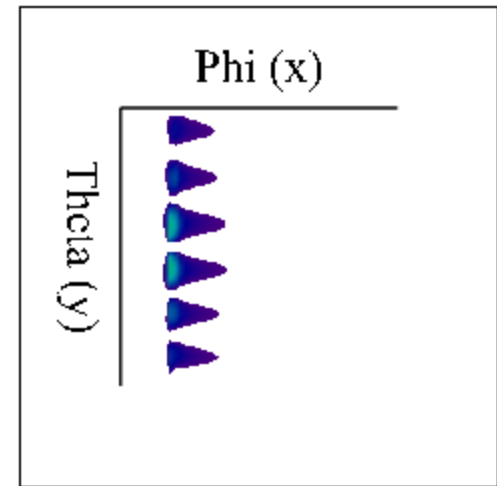
X-Polarization Results



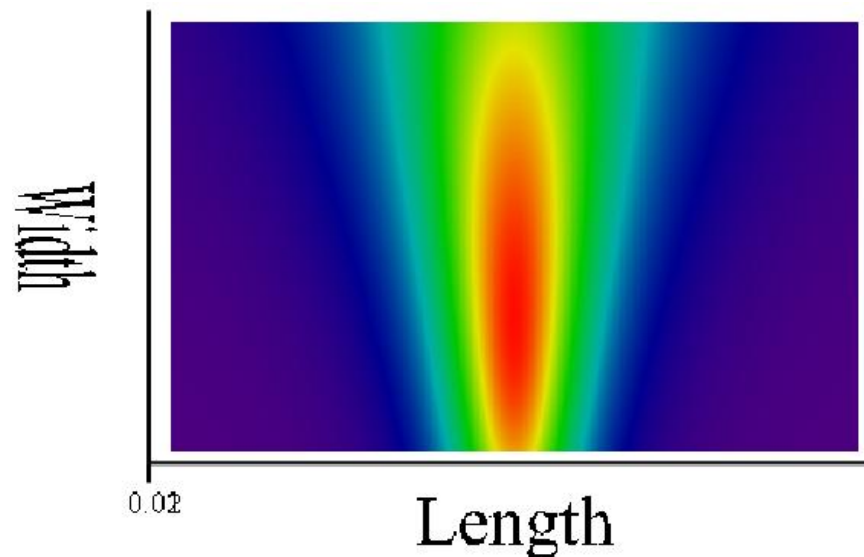
eMagLog



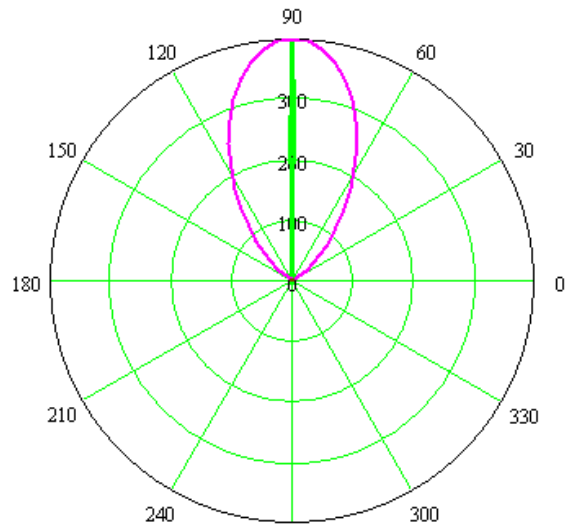
eDecLog



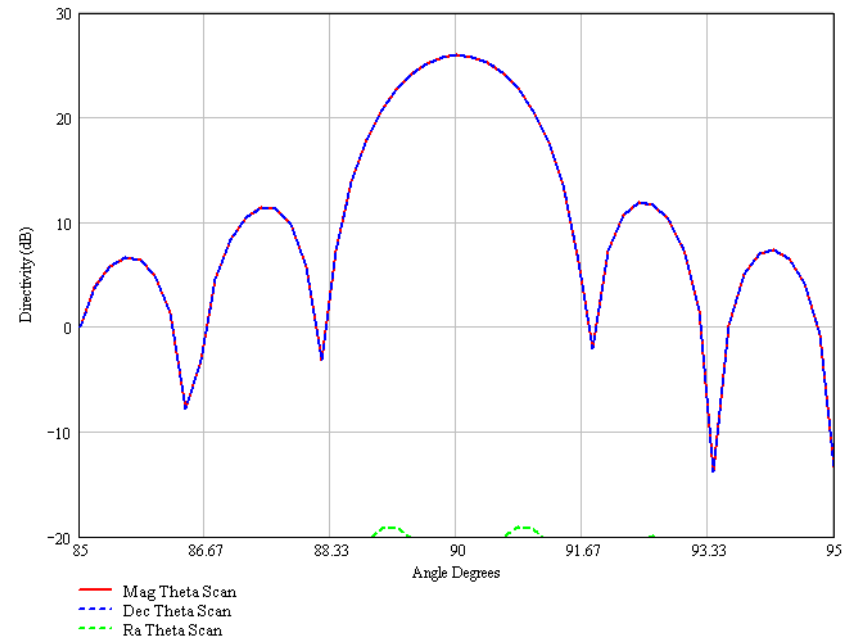
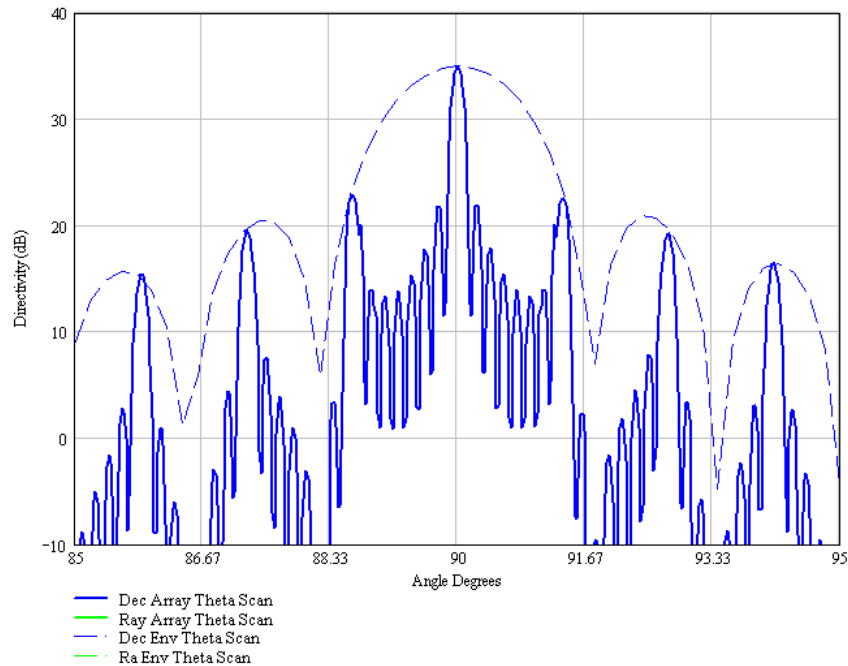
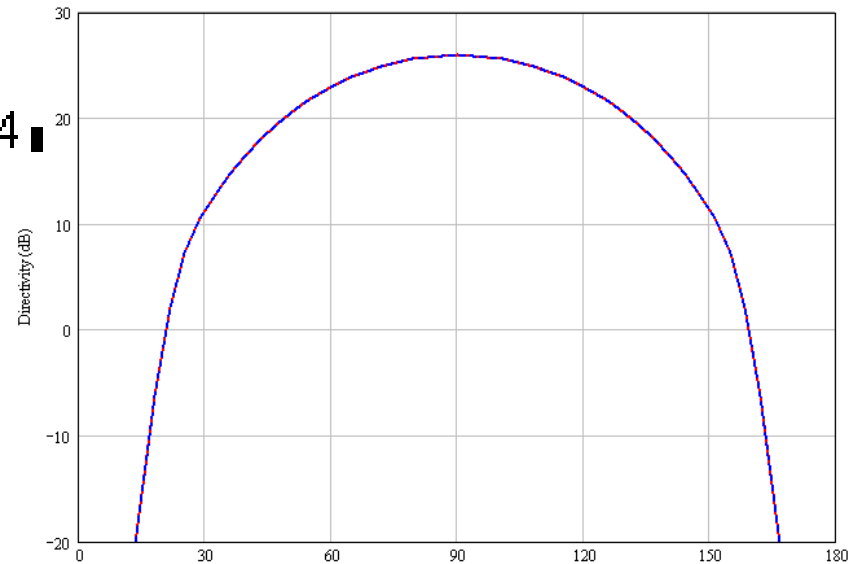
eRaLog



X-Polarization Results



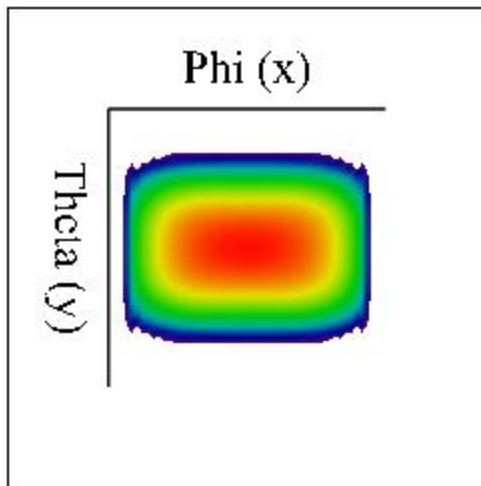
$$\frac{L_{em}}{\lambda} = 0.944$$



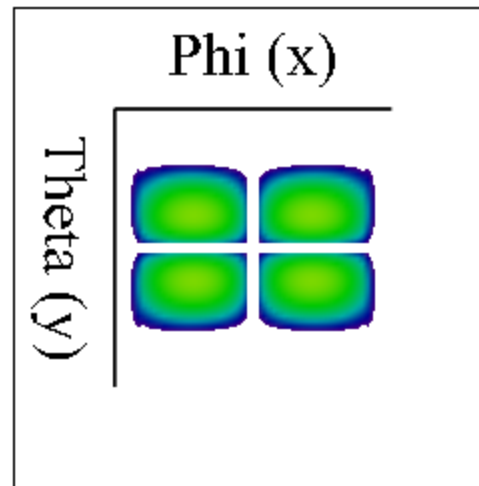
Future Work

- Explore other feed designs
 - Square patch antenna
 - Folded dipole
- Moment Method simulation of feed to understand coupling
- Explore larger f-ratio

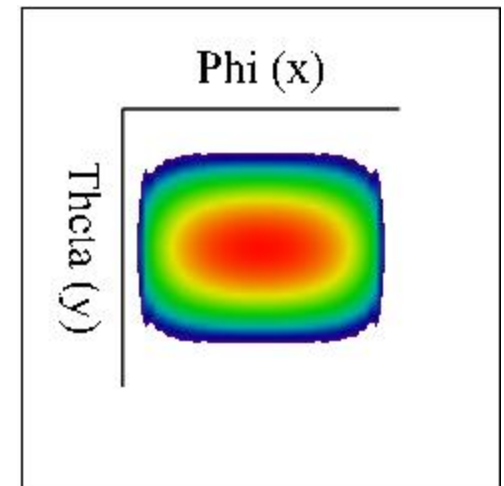
Y Polarization (Full Width)



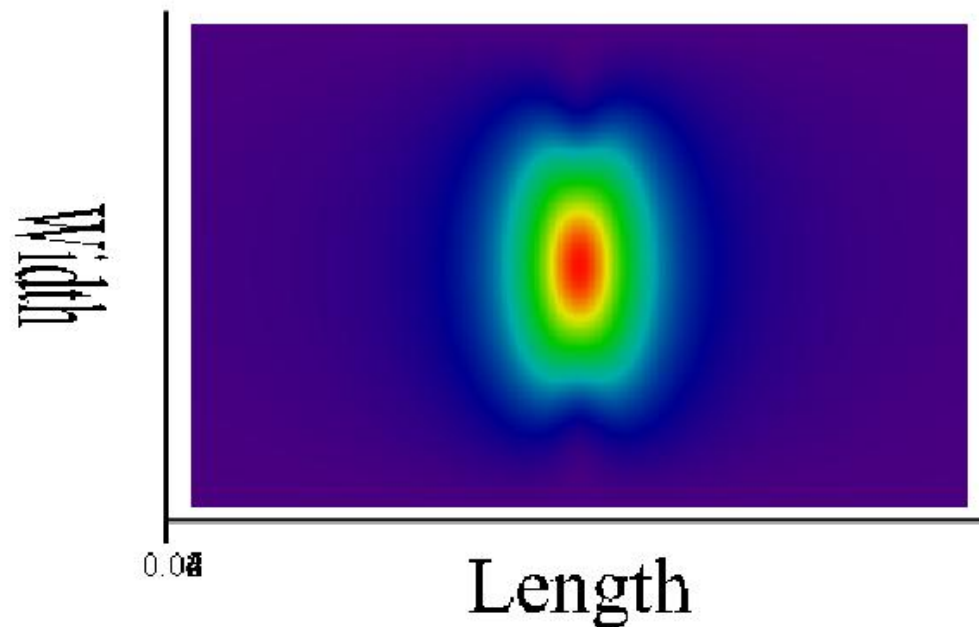
eMagLog



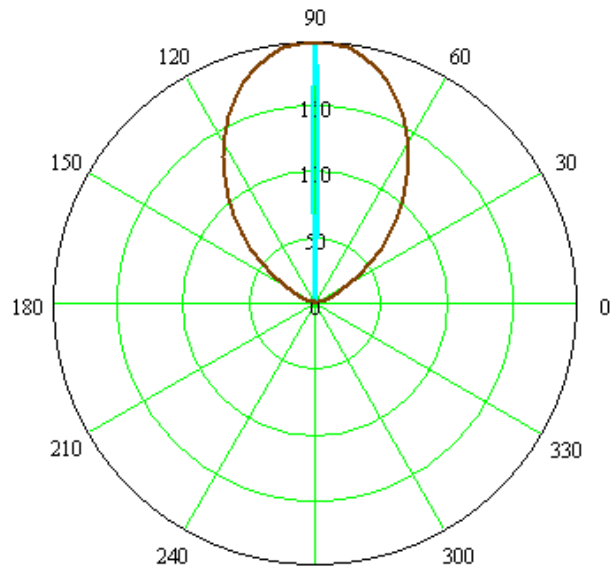
eDecLog



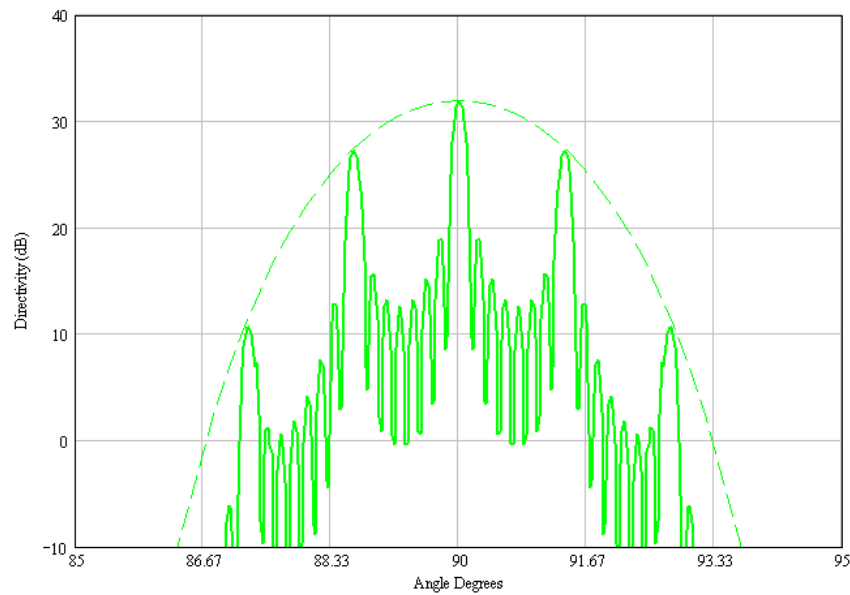
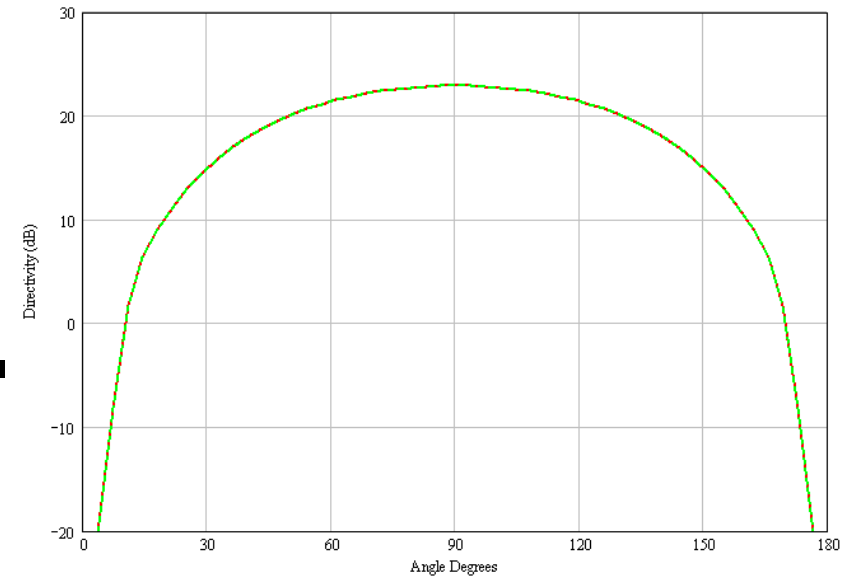
eRaLog



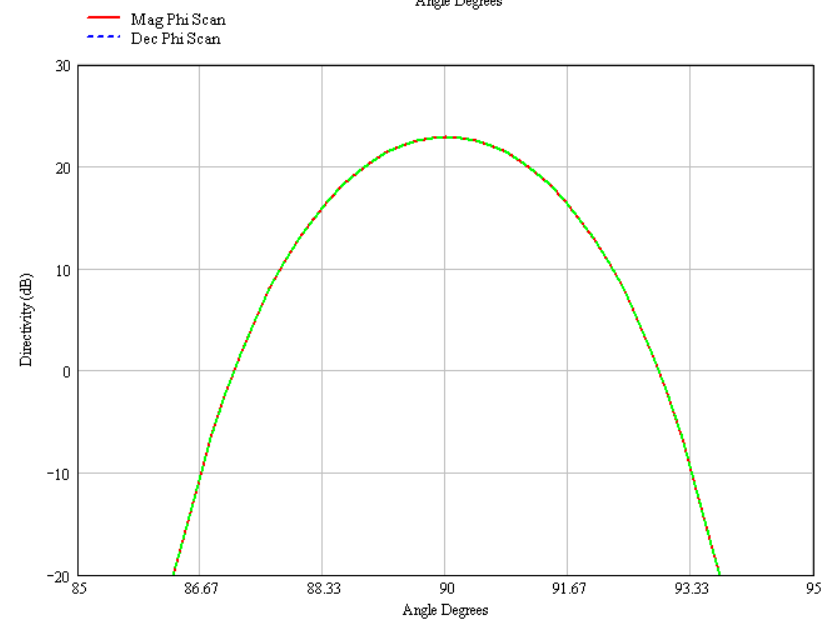
Y Polarization (Full Width)



$$\frac{L_{em}}{\lambda} = 0.376$$

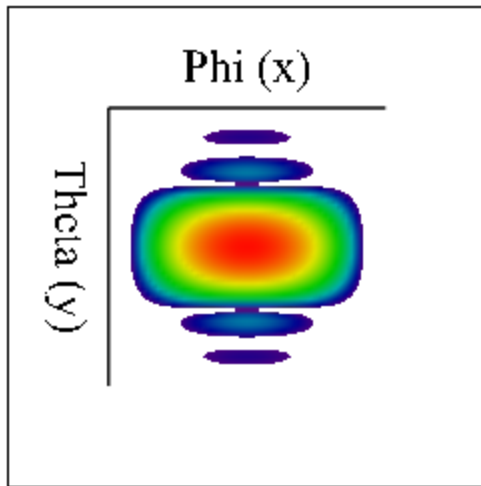


Dec Array Theta Scan
 Ray Array Theta Scan
 Dec Env Theta Scan
 Ra Env Theta Scan

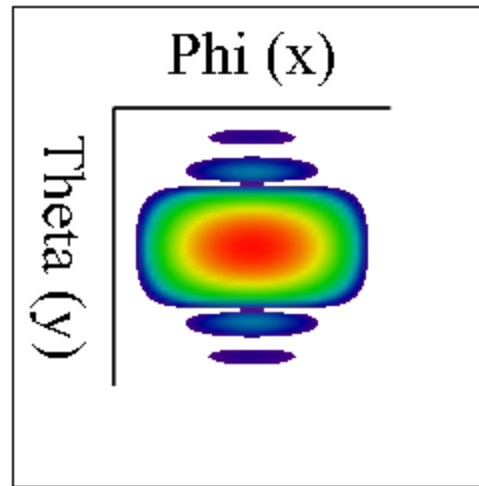


Mag Phi Scan
 Dec Phi Scan

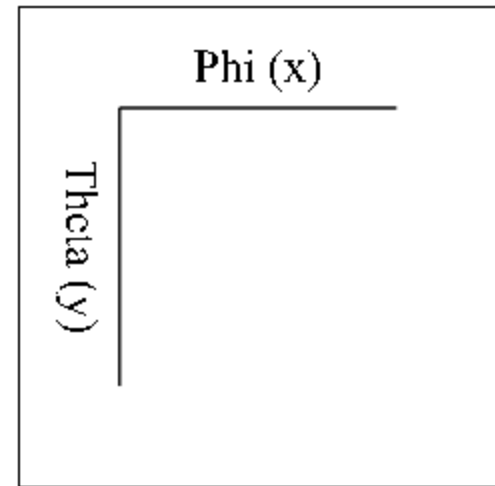
X Polarization (Full Width)



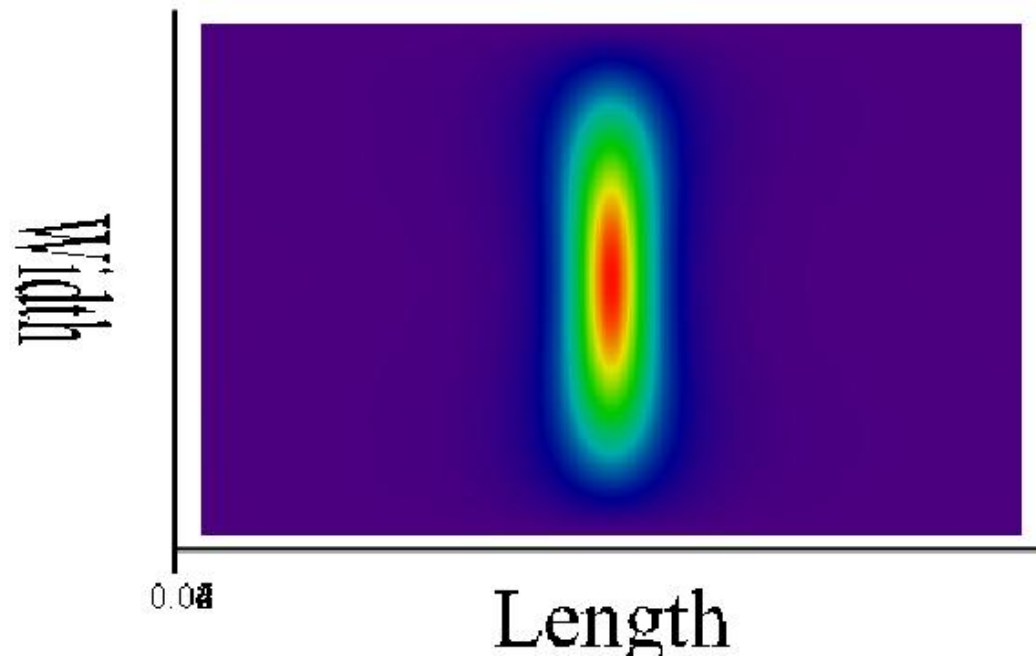
eMagLog



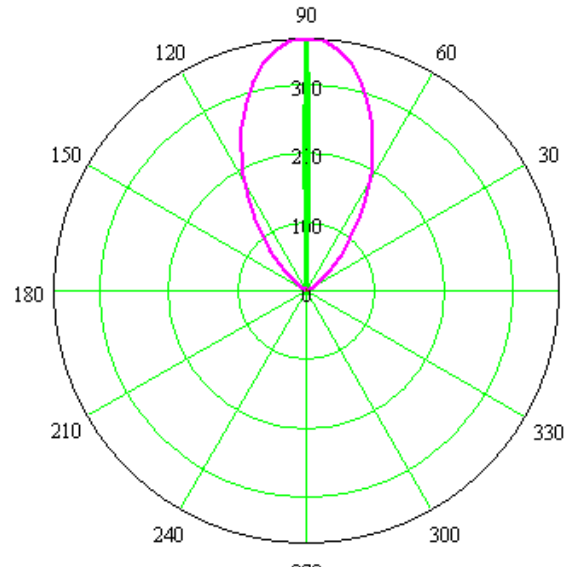
eDecLog



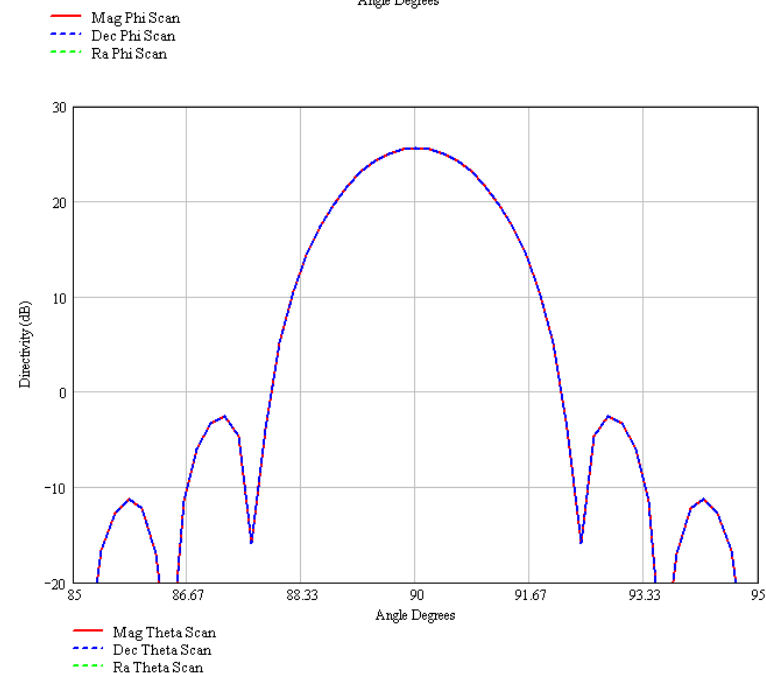
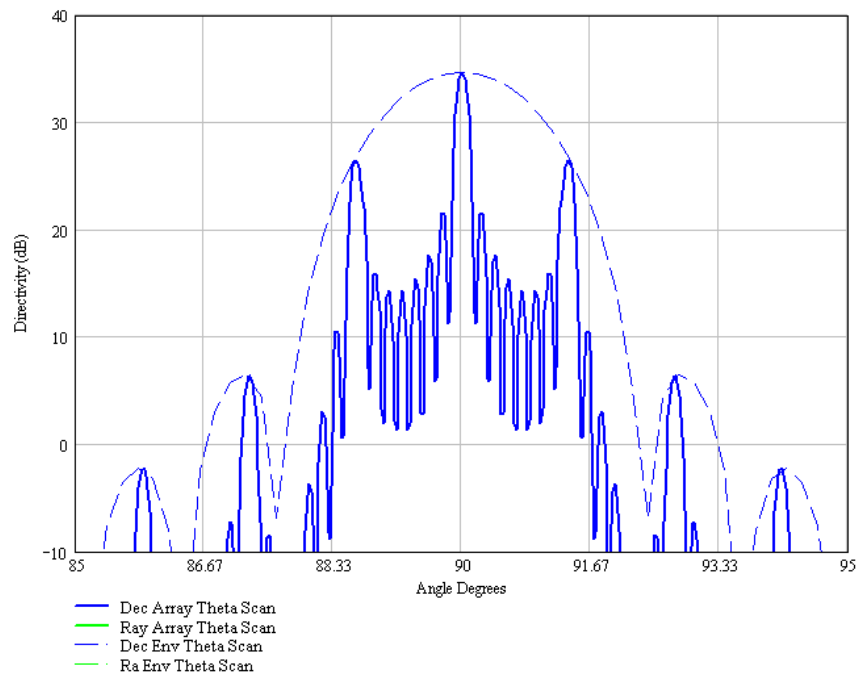
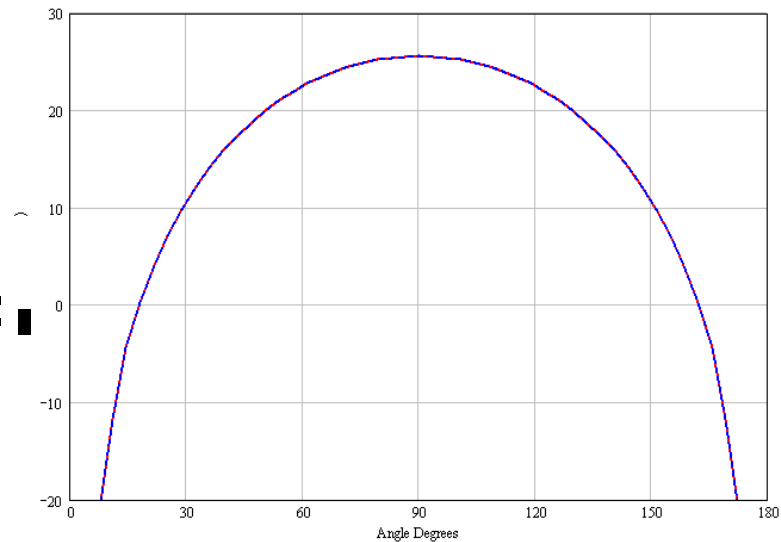
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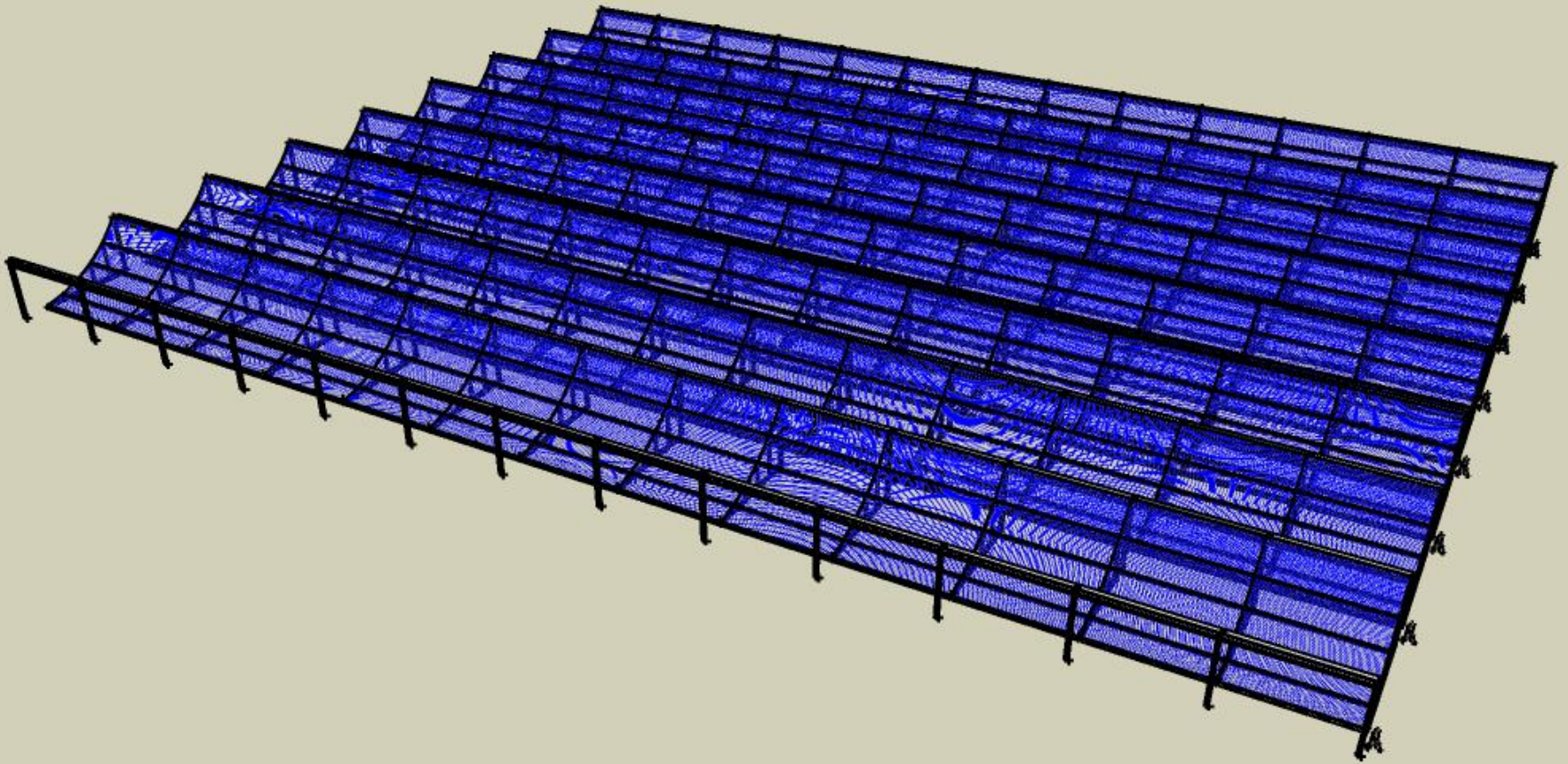
X Polarization (Full Width)



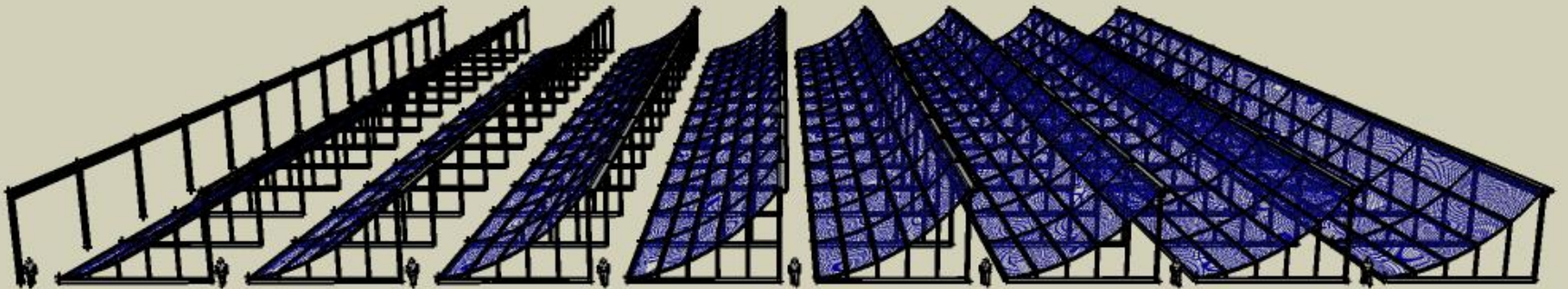
$$\frac{L_{em}}{\lambda} = 0.698$$



Telescope Layout



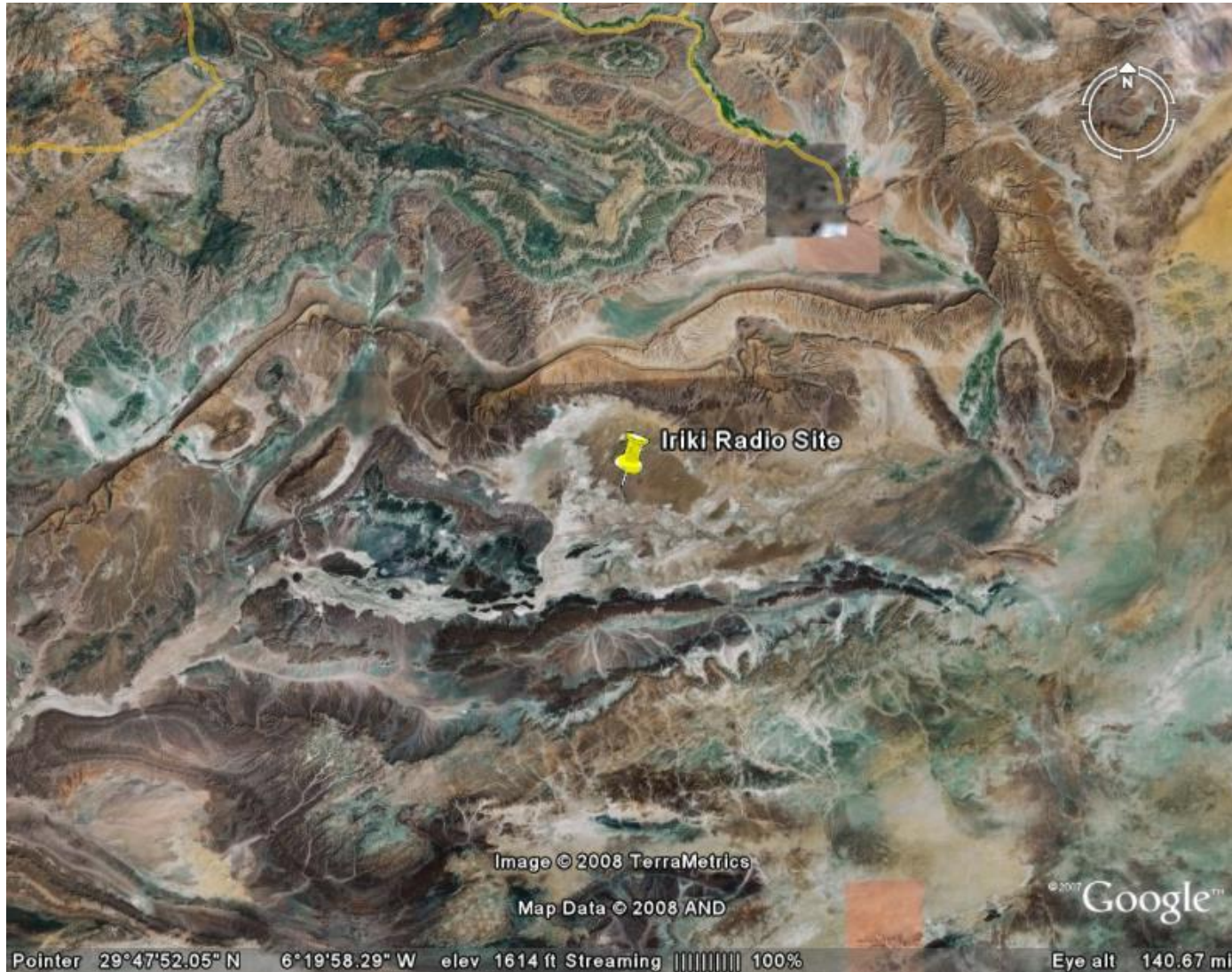
Telescope Layout



Iriki Dry Lake Site



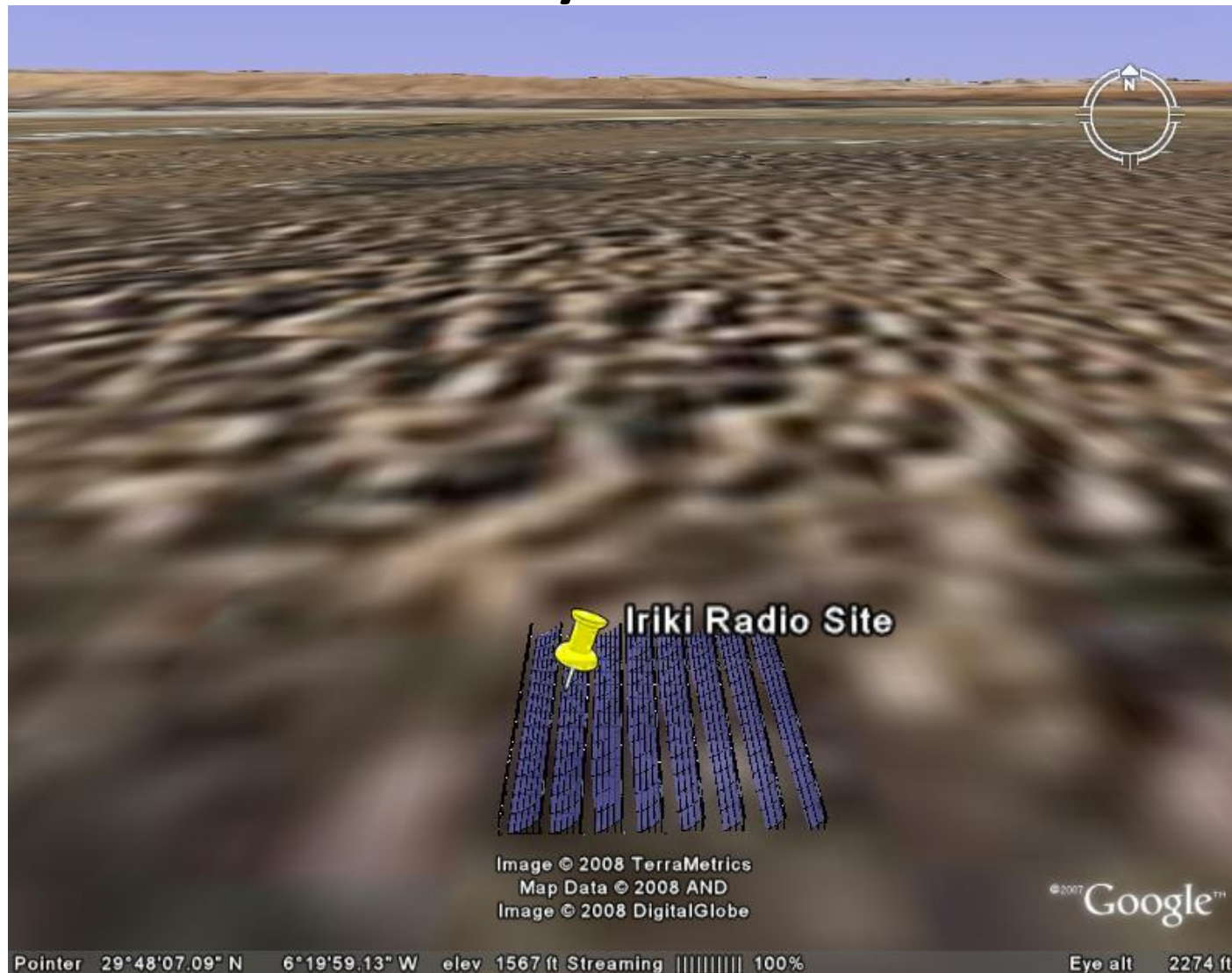
Iriki Dry Lake Site



Iriki Dry Lake Site



Iriki Dry Lake Site



Iriki Dry Lake Site

